

HOW WELL DOES ORIGEN PREDICT SPENT LWR FUEL CHARACTERISTICS?

J. C. Mailen and J. W. Roddy
Chemical Technology Division
Oak Ridge National Laboratory
Oak Ridge, Tennessee 37831

ABSTRACT

The ORIGEN computer code is widely used to estimate the radionuclide content (actinides, activation and fission products) of irradiated reactor fuel and the resultant heat generation and radiation levels associated with such fuel. These estimates are used as source terms in safety evaluations of operating reactors, for evaluation of fuel behavior and regulation of the at-reactor storage, for transportation studies, and for evaluation of the ultimate geologic storage of the fuel.

Calculated values determined using several variations of ORIGEN have been compared with experimentally determined values for actual fuel for many, but not all, of the parameters desired. In most cases, the comparisons did not use the most recent ORIGEN2 program, the most recent data libraries, or currently required quality assurance (QA) procedures. Comparisons of fuel composition data with ORIGEN2 are very limited, and the only data with proper QA are currently being acquired by Battelle Pacific Northwest Laboratory.

This survey summarizes the fuel data available in the open literature and, where given, the calculated values by ORIGEN. Plans for additional analyses of well-characterized reactor fuel samples to improve the validation of ORIGEN2 are discussed.

INTRODUCTION

ORIGEN and derivative programs are used throughout the world to estimate the actinide, fission product, and activation product contents of irradiated reactor fuels and the resultant heat generation and radiation levels associated with such fuels. These estimates are used as source terms in safety evaluations of operating reactors, for assessment of fuel behavior and regulation of the storage at the reactor, for transportation studies, and for evaluation of the ultimate geologic storage of the fuel. ORIGEN2 (1,2), a revised and updated version of ORIGEN, is an important code for formulating these predictions since it is currently used by many groups, including utilities, the U.S. Department of Energy (DOE), and the U.S. Nuclear Regulatory Commission (NRC), for such calculations.

The predictions of ORIGEN2 have not been adequately compared with experimental data for all fuel characteristics. This paper briefly summarizes the existing comparisons of experimental data with ORIGEN, with particular emphasis on the composition of irradiated fuel.

DESCRIPTION OF ORIGEN2

ORIGEN2 is a versatile computer code for calculating the nuclear composition and characteristics of fission reactor fuel. The input data bases include reactor-dependent cross sections, decay data (decay half-lives and branching fractions, internal transitions, etc.), fission product yields, photon production rates and energies, and neutron production rates. The current version of ORIGEN2 contains cross-section libraries for seven types of reactors. The user must specify the type of reactor, initial material composition, irradiation history, and decay history. ORIGEN2 contains three data bases comprising separate categories of nuclides: 130 actinides, 850 fission products,

and 720 activation products. Several of the nuclides appear in more than one category. The code can predict the composition (g or g-atom), radioactivity (Ci), and the thermal power (W) for each of the nuclides. In addition, the neutron generation rates from alpha-neutron reactions and spontaneous fission and the photon production rates from gamma rays, X-rays, bremsstrahlung, etc., can be obtained. The results are presented in a tabular form. ORIGEN2 is written in the FORTRAN language and was developed for mainframe computers, such as the IBM, UNIVAC, CDC 7000 series, and CRAY and has also been used on "minicomputers," such as the VAX and DEC. A version is being tested for the IBM PC-AT microcomputer. The ORIGEN2 program is readily available to all users through the Oak Ridge National Laboratory/Radiation Shielding Information Center (ORNL/RSIC).

WHY VALIDATE ORIGEN?

Better estimates of the radioactive composition of the fuel, through improvements in the predictive capability of ORIGEN2, would be important in waste packaging, transportation, and fuel handling, where substantial savings in fabrication and operation costs could be possible. Although the actual amounts cannot be quantified, the incremental costs to one portion of the repository system will be discussed as an example.

The U.S. Department of Energy (DOE) (3) has performed an analysis of the waste management costs for the Davis Canyon site. The estimates for shipping spent fuel are ~\$2 billion, while the number of casks required for shipment is 156 ± 22 by truck and 96 ± 15 by rail. Capital costs for each truck and rail cask are estimated to be \$1.5 million and \$2.5 million, respectively. If a completely validated version of ORIGEN2 results in an expenditure of \$1 million, the incremental cost would be <0.1% of the total capital cost for the casks and would have a negligible effect

*Operated by Martin Marietta Energy Systems, Inc., for the U.S. Department of Energy under Contract No. DE-AC05-84OR21400.

on the total shipping costs. The benefits of greater ORIGEN2 accuracy would be reduced design margins and lower cask weights, which would result in lower construction and hauling costs. An identical scenario can be made for the waste repository and monitored retrievable storage facilities, in which shielding thicknesses and heat-removal requirements can be reduced.

Another benefit of a successful validation effort that cannot be quantified is the assurance that the methodology is the most current, the data bases are up to date, and the program contains no major flaws. Deficiencies in any of these areas would have a serious impact on the acceptability of the code results for design and licensing, resulting in expensive delays or facility modifications.

COMPARISON OF ORIGEN PREDICTIONS WITH EXPERIMENTAL RESULTS

Values determined using several variations of ORIGEN have been compared with those determined for actual fuel for many, but not all, of the parameters desired. In most cases, the comparison was not made with the most recent ORIGEN2 program (2), the most up-to-date nuclear data libraries, or currently required quality assurance (QA) procedures. An earlier summary has been published (2) in which heat generation rates, actinide contents, and krypton and xenon isotope contents of irradiated fuels are compared with values calculated using ORIGEN2.

In this report, the main effort has been to assemble the existing comparisons of experimental reactor fuel compositions with those predicted by ORIGEN, since predictions of composition are required as input to calculations of heat and radiation generation. This effort has additional value, since the fuel composition data had not been completely surveyed in the past. The available comparisons of heat and radiation generation by fuel assemblies with ORIGEN predictions will be summarized first, followed by the fuel composition comparisons.

Heat Generation

The experimental heat-generation data for fuel assemblies have been compared with those predicted using ORIGEN2 (4-11). Comparisons of measured values with those predicted by ORIGEN agree to within $\pm 10\%$; the experimental data scatter is also $\pm 10\%$. The data cover only a limited number of cooling times and burnups.

Gamma Rates

Gamma exposure rates have been measured near full fuel bundles in a pool experiment (12) and surrounding a partially and fully loaded spent fuel storage cask (8,11). In both cases, a combination of an ORIGEN code for prediction of the photon source and a radiation transport code were required; this makes it impossible to completely separate experimental errors from inaccuracies introduced by the codes. Further, inaccuracies introduced by the individual codes cannot be determined. Strickler (12) found reasonable agreement (a factor of 2) between the predicted [ORIGEN and QAD-F (3)] and the measured values for locations near the sides of the fuel; however, there were large discrepancies (greater than an order of magnitude) when the codes were applied to locations above the fuel. Wiles (11) found the predictions [ORIGEN and QAD-CG (14)] agreed well with measured data over the length of the neutron shield, but, above and below the ends of

the shield, dose rate peaks were underpredicted by a factor of 2. The discrepancies between the predictions and measurements could have been due to the predicted quantities of radioisotopes by ORIGEN (or ORIGEN2), from approximations within the geometric codes (QAD-F or QAD-CG), from errors in the experiment, or from inaccuracies in the assumed fuel attributes.

Neutron Rates

Neutron dose rate measurements were made on the same partially and completely filled storage cask as was used for gamma measurements (8,11). The absolute neutron source strength was based on ORIGEN2 values calculated for each assembly, and the resulting dose rates were computed for the cask outer surface utilizing the DOT computer code (15). The predicted neutron dose rates on the ends and side of the cask on which there is no neutron shield were a factor of ~ 2 to 6 higher than experimental data. Calculated neutron dose rates were a factor of ~ 2 higher than the experimental data on the side of the cask having shielding.

Composition Data

Fuel composition data were found for 16 reactors; a total of 295 analyses of fuel samples were identified, with 282 of these giving experimental contents of actinides and 265 giving experimental contents of fission products (16-48). It should be noted that 219 of the analyses were of pellet-sized samples from Yankee-Rowe (38), which used stainless-steel clad fuel. A complete report presenting data sources and surveying the currently available data for all the parameters (90 references) is in preparation (49).

Data comparing experimental fuel compositions with ORIGEN predictions were found only for the H. B. Robinson (18,19,22,23,26,30,47,48), Oconee-1 (20,26), BR3 (39), and Turkey Point-3 (45) reactors. Table I gives the high and low ratios of the experimentally determined radioactive concentration in irradiated fuel to the values calculated by ORIGEN, the number of comparisons found, the average ratios, and the standard deviations for all isotopes for which usable data were found. The values in this table are only indicative of the ability of ORIGEN to predict various nuclide concentrations in irradiated fuel and must be used with caution, since most studies did not use current QA standards, some nuclides are difficult to analyze, and the more recent ORIGEN2 code yields better agreement in some areas. Isotopes that are difficult to determine in irradiated light-water reactor (LWR) fuel include: (1) tritium, of which $\sim 50\%$ is in the Zircaloy cladding, which is often not analyzed; (2) ^{106}Ru , a portion of which is not readily soluble in the nitric acid commonly used for dissolving irradiated fuel; (3) ^{129}I , which must be volatilized from the fuel solution, trapped, and determined by neutron activation; and (4) ^{14}C , which must be volatilized from the fuel solution and trapped. Data from experiments in which the experimental procedures did not ensure nearly complete recovery of these isotopes were not included in the compiled data. Experimental errors can also arise from errors in sampling or equipment calibration. ORIGEN2 predictions that are an improvement over earlier versions of the code include much better agreement with the limited data for higher actinides (2). Uncertainties in the chemical analyses and experimental difficulties would be expected to result in a large range of ratios and standard deviations, such as those found for ^{242}Cm , ^{244}Cm , ^{129}I , ^{106}Ru , ^{241}Am , ^3H , and ^{125}Sb . The large scatter found for ^{134}Cs and ^{144}Ce is difficult to explain, since these isotopes should be relatively easy to measure.

TABLE I

Average Ratios^a (Experiment/ORIGEN)

Isotope	High/Low	No. ^b	Average	SDC
³ H	0.58/0.81	3	0.81	0.18
¹⁴ C	1.14/1.09	2	1.06	
⁸⁵ Kr	1.29/1.39	3	1.34	0.04
⁷⁹ Se	0.13/0.13	2	0.13	
⁹⁰ Sr	0.81/1.04	4	0.94	0.08
⁹⁹ Tc	0.52/0.95	7	0.84	0.14
¹⁰⁶ Ru	0.75/1.15	4	0.92	0.17
¹²⁵ Sb	0.50/0.91	3	0.67	0.18
¹²⁶ Sn	0.23/0.23	2	0.23	
¹²⁹ I	0.43/1.74	11	0.80	0.32
¹³⁴ Cs	0.44/1.34	7	0.67	0.28
¹³⁷ Cs	0.81/1.04	13	0.98	0.11
¹⁴⁴ Ce	0.64/1.29	7	0.92	0.19
¹⁵⁴ Eu	0.28/0.29	2	0.28	
²³⁴ U	0.92/1.10	8	1.10	0.10
²³⁵ U	0.86/1.16	17	1.01	0.07
²³⁶ U	0.95/1.09	17	1.01	0.07
²³⁷ Np	0.92/1.03	4	0.98	0.05
²³⁸ Pu	0.78/1.27	21	1.15	0.15
²³⁹ Pu	0.84/1.03	18	0.97	0.05
²⁴⁰ Pu	0.87/1.12	18	1.03	0.07
²⁴¹ Pu	0.77/1.21	18	0.97	0.10
²⁴² Pu	0.94/1.73	14	1.12	0.22
²⁴¹ Am	0.27/0.946	9	0.77 ^d	0.25
²⁴² Am	---	1	0.99	
²⁴³ Am	---	1	0.92	
²⁴² Cm	1.08/3.28	7	1.69 ^d	0.68
²⁴³ Cm	---	1	0.95	
²⁴⁴ Cm	0.40/1.12	7	0.70 ^d	0.31
²⁴⁵ Cm	---	1	1.25	
²⁴⁶ Cm	---	1	1.04	
²⁴⁷ Cm	---	1	1.00	
²⁴⁸ Cm	---	1	0.95 ^d	

^aRatios of absolute concentrations.^bNumber of determinations.^cStandard deviation.^dThe latest calculations using ORIGEN2 gave ratios of 1.05, 1.12, and 0.99 for ²⁴¹Am, ²⁴²Cm, and ²⁴⁴Cm, respectively. The ²⁴⁸Cm single data point had poor statistics.

The data in Table I can be divided into nuclides which have relatively good agreement (within ±10%), moderately good agreement (within ±50%), and poor agreement between the experimental data and the ORIGEN predictions, as shown in Table II. The extent to which the disagreements are due to inaccuracies in ORIGEN calculations (possibly from nuclear data libraries or reactor models), experimental limitations, or analytical inaccuracies cannot be easily determined unless replicate measurements are made using well-characterized fuel samples and approved QA procedures (e.g., analytical techniques, sample traceability).

PROBLEMS WITH EXPERIMENTAL DATA

The experimental data on heat and radiation-generation rates from irradiated LWR fuel are presumed adequate. Agreement between experimental and predicted heat-generation rates is excellent for early time periods. Additional efforts in radiation (gamma and neutron) rates should address the radiation transport

TABLE I.

Relative Agreement of Experimental Data and ORIGEN Predictions for Various Isotopes

Excellent (within ±10%)	Fair (within ±50%)	Poor (>50%)
²³⁴ U	²³⁸ Pu	⁷⁹ Se
²³⁵ U	²⁴² Pu	¹²⁶ Sn
²³⁶ U	²⁴² Cm ^a	¹⁵⁴ Eu
²³⁷ Np	²⁴⁵ Cm ^a	
²³⁹ Pu	³ H	
²⁴⁰ Pu	⁸⁵ Kr	
²⁴¹ Pu	⁹⁹ Tc	
²⁴¹ Am	¹²⁹ I	
²⁴² Am ^a	¹²⁵ Sb	
²⁴³ Am ^a	¹³⁴ Cs	
²⁴⁴ Cm ^a	¹⁴⁴ Ce	
²⁴⁶ Cm ^a		
²⁴⁷ Cm ^a		
¹⁴ C		
⁹⁰ Sr		
¹⁰⁶ Ru		
¹³⁷ Cs		

^aOnly one experimental determination.

calculations, since the codes used in the reported studies were relatively inaccurate.

Comparisons of fuel composition data with ORIGEN2 are very limited, and the only data with proper QA are being currently acquired by Battelle Pacific Northwest Laboratory (32,50). In most cases, the other comparisons did not use the most recent ORIGEN2 program, the most recent data libraries, or currently required QA procedures. Many of the earlier data were used in the development of the ORIGEN codes and cannot be used for validation efforts. A significant additional effort is needed to adequately validate ORIGEN2 for the prediction of fuel compositions.

FUTURE STUDIES

Work is currently under way at PNL in the Materials Characterization Center (33,50) to obtain well-characterized LWR fuel for use in studies related to fuel storage in geologic repositories. The availability of portions of these well-characterized fuel samples from PNL makes this an ideal time to validate the ORIGEN2 code. A spark-source mass spectrometer (SSMS) at ORNL, which is capable of analyzing fully irradiated fuel samples, will make it possible to examine isotopes which are difficult to determine using standard radiochemical techniques.

The identification of the important isotopes that need to be predicted in spent fuel is being undertaken by assembling the recommendations of personnel in the waste project repository offices, those performing criticality calculations, and experts in the use of the ORIGEN2 code. These recommendations, along with information on analytical capabilities and funding availability, will be used to define a program to improve the validation of ORIGEN-type programs. New analyses resulting from such a program will allow the validation of the ORIGEN2 code required for its use in future years. The data base generated will also be available for development or validation of other similar codes.

REFERENCES

1. M. J. Bell, "ORIGEN - The ORNL Isotope Generation and Depletion Code," ORNL-4628, Oak Ridge National Laboratory (1973).
2. A. G. Croff, "ORIGEN2: A Versatile Computer Code for Calculating the Nuclide Compositions and Characteristics of Nuclear Materials," Nucl. Technol., 62, 335 (1983).
3. "Environmental Assessment: Davis Canyon Site, Utah," DOE/RW-0071, Vol. II, App. A, U.S. Department of Energy (1986).
4. F. Schmittroth, "ORIGEN2 Calculations of PWR Spent Fuel Decay Heat Compared With Calorimeter Data," HEDL-TME 83-32, Hanford Engineering Development Laboratory (1984).
5. F. Schmittroth, "ORIGEN2 Calculations of PWR Spent Fuel Decay Heat Compared with Calorimeter Measurements," Proc. Fuel Reprocessing and Waste Management, Jackson, Wyoming, August 26-29, 1984, p. 2-69, American Nuclear Society (1984).
6. J. M. Creer, "Decay Heat and Heat Transfer Predictions for Spent Fuel Storage Systems," PNL-SA--12658, Pacific Northwest Laboratory (1984).
7. H. R. Strickler and J. W. Doman, "In-Plant Test Measurements for Spent Fuel Storage at Morris Operation. Volume 3: Fuel Bundle Heat Generation Rates," NEDG-24922-3, General Electric Co. (1982).
8. M. A. McKinnon et al., "Monticello BWR Spent Fuel Assembly Decay Heat Predictions and Measurements," PNL-5799, Pacific Northwest Laboratory (1986).
9. J. M. Creer and J. W. Shupe, Jr., "Development of a Water Boil-Off Spent Fuel Calorimeter System," PNL-3434, Pacific Northwest Laboratory (1981).
10. M. A. McKinnon et al., "BWR Spent Fuel Storage Cask Performance Test, Volume I. Pre- and Post-Test Decay Heat, Heat Transfer, and Shielding Analyses," PNL-5777 Vol. I, Pacific Northwest Laboratory (1986).
11. L. E. Wiles et al., "BWR Spent Fuel Storage Cask Performance Test, Volume II. Pre- and Post-Test Decay Heat, Heat Transfer, and Shielding Analyses," PNL-5777 Vol. II, Pacific Northwest Laboratory (1986).
12. H. R. Strickler and K. J. Eger, "In-Plant Test Measurements for Spent Fuel Storage at Morris Operation," NEDG-24922-2, General Electric Co. (1981).
13. R. E. Malenfant, "QAD: A Series of Point-Kernel General-Purpose Shielding Programs," LA-3573, Los Alamos Scientific Laboratory (1967).
14. "QAD-CG: A Combinatorial Geometry Version of QAD-P5A, a Point-Kernel Code for Neutron and Gamma-Ray Shielding Calculations," CCC-307, Radiation Shielding Information Center, Oak Ridge National Laboratory, current listing.
15. W. A. Rhoades and R. L. Childs, "An Updated Version of the DOT-4 One- and Two-Dimensional Neutron/Photon Transport Code," ORNL-5851, Oak Ridge National Laboratory (1982).
16. W. B. Wilson, R. J. LaBauve, and T. R. England, "Calculations of Spent Thermal Reactor Fuel Nuclide Inventories and Comparisons with Measurements," Proc. Thermal Reactor Benchmark Calculations, Techniques, Results, and Applications, Upton, New York, May 17-18, 1982, NP-2855, p. 8-1 (1983).
17. D. R. Johnson and J. A. Stone, "Light Water Reactor Fuel Reprocessing: Dissolution Studies of Voloxidized and Nonvoloxidized Fuel," DP-1520, Savannah River Laboratory (1980).
18. J. H. Goode and R. G. Stacy, "Head-End Reprocessing Studies with H. B. Robinson-2 Fuel," ORNL/TM-6037, Oak Ridge National Laboratory (1978).
19. J. H. Goode, R. G. Stacy, and V. C. A. Vaughen, "Head-End Studies of H. B. Robinson-2 Fuel: II. Parametric Voloxidation Studies," ORNL/TM-6888, Oak Ridge National Laboratory (1980).
20. J. H. Goode, R. G. Stacy, and V. C. A. Vaughen, "Comparison Studies of Head-End Reprocessing Using Three LWR Fuels," ORNL/TM-7103, Oak Ridge National Laboratory (1980).
21. D. O. Campbell et al., pp. 6-16 of "LWR Fuel Reprocessing and Recycle Program Quarterly Report for Period January 1 to March 31, 1976," B. L. Vondra, program manager, ORNL/TM-5447, Oak Ridge National Laboratory (1976).
22. D. O. Campbell et al., pp. 10-31 of "LWR Fuel Reprocessing and Recycle Program Quarterly Report for Period April to June 30, 1976," B. L. Vondra, program manager, ORNL/TM-5547, Oak Ridge National Laboratory (1976).
23. D. O. Campbell pp. 23-38 of "LWR Fuel Reprocessing and Recycle Program Quarterly Report for Period July 1 to September 30, 1976," B. L. Vondra, program manager, ORNL/TM-5660, Oak Ridge National Laboratory (1976).
24. D. O. Campbell et al., pp. 13-40 of "LWR Fuel Reprocessing and Recycle Program Quarterly Report for Period October 1 to December 31, 1976," B. L. Vondra, program manager, ORNL/TM-5760, Oak Ridge National Laboratory (1977).
25. D. O. Campbell et al., pp. 2-6 to 2-25 of "LWR Fuel Reprocessing and Recycle Program Quarterly Report for Period January 1 to March 31, 1977," B. L. Vondra, program manager, ORNL/TM-5864, Oak Ridge National Laboratory (1977).
26. D. O. Campbell et al., pp. 2-15 to 2-32 of "LWR Fuel Reprocessing and Recycle Program Quarterly Report for Period April 1 to June 30, 1977," B. L. Vondra, manager, ORNL/TM-5987, Oak Ridge National Laboratory (1977).
27. D. O. Campbell et al., pp. 2-13 to 2-41 of "Alternate Fuel Cycle Technologies Program Quarterly Report for Period July 1 to September 30, 1977," B. L. Vondra, program manager, ORNL/TM-6076, Oak Ridge National Laboratory (1977).
28. D. O. Campbell et al., pp. 2-8 to 2-16 of "Alternate Fuel Cycle Technologies/Thorium Fuel Cycle Technology Programs Quarterly Report for Period October 1 to December 31, 1977," B. L. Vondra, program manager, ORNL/TM-6206, Oak Ridge National Laboratory (1978).
29. D. O. Campbell et al., pp. 2-6 to 2-9 of "Alternate Fuel Cycle Technologies/Thorium Fuel Cycle Technology Programs Quarterly Report for Period January 1 to March 31, 1978," B. L. Vondra, program manager, ORNL/TM-6307, Oak Ridge National Laboratory (1978).

30. D. O. Campbell et al., pp. 2-6 to 2-9 of "Alternate Fuel Cycle Technologies/Thorium Fuel Cycle Technology Programs Quarterly Report for Period April 1 to June 30, 1978," B. L. Vondra, program manager, ORNL/TM-6429, Oak Ridge National Laboratory (1978).
31. D. O. Campbell and W. L. Pattison, "The Effect of Heat Treatments on Tritium Volatility and the Behavior of Other Radioactive Constituents in Irradiated Fuel," ORNL/TM-7326, Oak Ridge National Laboratory (1981).
32. D. O. Campbell, Oak Ridge National Laboratory, personal communication of unpublished data to J. C. Mailen, Oak Ridge National Laboratory (March 1986).
33. J. O. Barner, "Characterization of LWR Spent Fuel MCC-Approved Testing Material - ATM-101," PNL-5109 Rev. 1, Pacific Northwest Laboratory (1985).
34. J. C. Ryman, O. W. Hermann, C. C. Webster, and C. V. Parks, "Fuel Inventory and Afterheat Power Studies of Uranium-Fueled Pressurized Water Reactor Fuel Assemblies Using the SAS2 and ORIGEN-S Modules of Scale with an ENDF/B-V Updated Cross Section Library," NUREG/CR-2397 (ORNL/CSD-90), Oak Ridge National Laboratory (1982).
35. C. M. Heeb et al., "Analysis of Alternative Light Water Reactor (LWR) Fuel Cycles," PNL-2792, Pacific Northwest Laboratory (1979).
36. M. H. Montgomery, Babcock & Wilcox, letter report to B. L. Vondra, Oak Ridge National Laboratory (April 5, 1978).
37. J. A. Baumgartner, "BWR Fuel Bundle Extended Burnup Program; Final Report," DOE/ET/34031-18, General Electric Company and Northern States Power Company (1984).
38. R. J. Nodvik, "Evaluation of Mass Spectrometric and Radiochemical Analyses of Yankee Core I Spent Fuel," WCAP-6068, Westinghouse Electric Corporation (1966).
39. N. Cadelli and M. Lippens, "Post-Irradiation Examination of Plutonium-Bearing Fuel Elements Irradiated in LWR Power Plants - A European Community Campaign," Proc. Specialists' Meeting, Improved Utilization of Water Reactor Fuel with Special Emphasis on Extended Burnups and Plutonium Recycling, Mol, Belgium, May 7-11, 1984, IWGFPT/20 (CONF-8405285), p. 182, International Atomic Energy Agency (1984).
40. J. P. Adams and B. R. Dabell, "Characteristics of UO₂-Zr Fuel Rods Irradiated in the BR3 Reactor; Draft Preliminary Report for Comment," EG&G Idaho, Inc. (November 1984).
41. U. Fischer and H. W. Wiese, "Improved and Consistent Determination of the Nuclear Inventory of Spent PWR Fuel on the Basis of Cell-Burnup Methods Using KORIGEN," KfK 3014 (ORNL-tr-5043, translation), Karlsruhe Nuclear Research Center (1983).
42. S. D. Atkin, "Destructive Examination of 3-Cycle LWR Rods from Turkey Point Unit 3 for the Climax - Spent Fuel Test," TC-1867, Hanford Engineering Development Laboratory (1980).
43. S. D. Atkin, "Destructive Examination of 3-Cycle LWR Fuel Rods from Turkey Point Unit 3 for the Climax-Spent Fuel Test," HEDL-TME 80-89, Hanford Engineering Development Laboratory (1981).
44. R. B. Davis and V. Pasupathi, "Data Summary Report for the Destructive Examination of Rods G7, G9, J8, I9, and H6 from Turkey Point Fuel Assembly B17," HEDL-TME 80-85, Hanford Engineering Development Laboratory (1981).
45. G. J. Neely and F. Schmittroth, "Decay-Heat and Gamma-Dose Rate Prediction Capability in Spent LWR Fuel," HEDL-TC-1787, Hanford Engineering Development Laboratory (1982).
46. D. C. Langstaff et al., "Examination of Stainless Steel-Clad Connecticut Yankee Fuel Assembly S004 After Storage in Borated Water," PNL-3828, Pacific Northwest Laboratory (1982).
47. J. L. McElroy, Pacific Northwest Laboratory, letter report to Jerry D. White, Richland Operations Office, Richland, Wash. (Nov. 7, 1985).
48. R. P. Wichner, Oak Ridge National Laboratory, memorandum to T. S. Kress, Oak Ridge National Laboratory, and L. Chan, U.S. Nuclear Regulatory Commission, "ORIGEN2 Description and Verification Status," (July 25, 1983).
49. J. W. Roddy and J. C. Mailen, "Radiological Characteristics of LWR Spent Fuel: A Literature Survey of Experimental Data," ORNL/TM-10105, Oak Ridge National Laboratory (in press).
50. J. O. Barner, "LWR Spent Fuel Approved Testing Materials for Radionuclide Release Studies," PNL-4686, Pacific Northwest Laboratory (1984).